

SPECIFICATION

PERMANENT MAGNET MOTOR

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TECHNICAL FIELD

The present invention relates to remedying cogging torque and improving torque linearity characteristics in permanent magnet motors having permanent magnets.

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BACKGROUND ART

A conventional permanent magnet motor will be described referring to Japanese Laid-Open Patent Publication 119175/1987. The permanent magnet motor (henceforth referred to as "surface magnet motor") such as this has a rotor provided with a plurality of permanent magnets fixed to the periphery of a rotary shaft, spacers between the permanent magnets, and pressing members formed of non-magnetic material for pressing radially on the surface of the permanent magnets.

In terms of this surface magnet motor, since the magnets are fixed to the surface of the rotor, the surface magnet motor has excellent torque linearity characteristics in terms of linearity between torque and current. Thus, under high load, large torque can be obtained with small current, providing excellent controllability.

However, the foregoing surface magnet motor requires the pressing members and associated components for fixing the permanent magnets, resulting in a complicated structure.

In order to solve the above mentioned problems, Japanese Laid-Open Patent Publication 197292/2000 discloses an interior permanent magnet motor.

In terms of the technology disclosed in the patent publication, the interior permanent magnet motor has rectangular, axially penetrating slots for the magnets, provided circumferentially in a rotor iron core at equal intervals in an amount for the number of poles of the rotor, with the long side of the slots oriented circumferentially along the iron core and the short sides oriented radially along the iron core, a permanent magnet being fixed in each of the magnet slots so that, with the magnetic-pole faces diametrically oriented in the iron core, neighboring magnetic poles are opposites, wherein the outer peripheral shape of the magnetic-pole portions of the rotor, formed along the magnetic-pole faces on the outer peripheral side of each of the permanent magnets, is such that each of the rotor magnetic-pole portions is arcuate so that, in the circumferentially central portion the distance from the iron core center is longest, and in the portions between poles the distance from the iron core center is shortest.

In terms of the interior permanent magnet motor, the permanent magnets are embedded in the stator iron core, so that the pressing members for fixing the permanent magnets are unnecessary.

However, in the interior permanent magnet in the above described Japanese Laid-Open Patent Publication 197292/2000, the thickness of the outer portion of the rotor iron core is not prescribed, so that a problem has been that the cogging torque—the torque variation that when no current is flowing occurs due to harmonic components of the air-gap magnetic flux

density—becomes somewhat large, and the torque linearity cannot be improved.

The present invention is intended to solve the above described problems and has as an object the provision of a permanent magnet motor
5 in which the cogging torque is lowered and the torque linearity is improved.

DISCLOSURE OF THE INVENTION

In a first aspect of the invention, a permanent magnet motor includes: a stator having a stator coil; and a rotor, having a plurality of
10 axially bored magnet slots, provided in an amount for the number of poles in the rotor iron core, permanent magnets being fixed into the magnet slots so that neighboring magnetic poles are opposites; wherein in the rotor, the outer peripheral shape of rotor magnetic-pole portions, formed along each magnetic-pole face on the outer peripheral side of the permanent magnets,
15 is formed so that, in a circumferentially central portion thereof, the distance from the center of the rotor iron core is longest, and, at the inter-polar space between a first of the permanent magnets and a second of the permanent magnets, the distance from the center of the rotor iron core is shortest, and so that the outermost surface of rotor magnetic-pole portions forms an arc,
20 each magnet slot, whose radially outer side approximately matches the arc, being bored in an approximate bow shape; and given that sheath thickness t_c formed by the outer-side surface of each permanent magnet and the outermost surface of each rotor magnetic-pole portion is approximately constant, and letting the thickness of each permanent magnet be the
25 magnet thickness t_m , then the relation $t_c/t_m \leq 0.25$ is satisfied.

According to the permanent magnet motor in this case, in comparison to conventional interior permanent magnet motors, an effect is realized in that the cogging torque is small and the torque linearity is improved.

5 In a second aspect of the invention, the permanent magnet motor satisfies the relation $0.143 \leq td/tm \leq 0.174$.

According to the permanent magnet motor in this case, the effect is realized of reducing the cogging torque even further.

10 In a third aspect of the invention, given that the diameter where the outer-side surface of the rotor is furthest from the center of the rotor iron core is the rotor maximum diameter Dr , and the radius of each arc formed by the outer-side surface of each of the rotor magnetic-pole portions is the rotor arc radius Rp , then the permanent magnet motor satisfies the relation $0.23 \leq Rp/Dr \leq 0.32$.

15 According to the permanent magnet motor, in the rotor in this case, the magnetic flux wave form, from the N (S) pole of the permanent magnet to the S (N) pole, approximates an ideal sinusoidal wave, so that the effect of reducing the cogging torque is obtained.

20 In a fourth aspect of the invention, given that the width of each of the magnet slots, corresponding to the thickness of each of the permanent magnets, is the slot width th , and with both ends of each of the magnet slots being provided with an approximately semi-circular surface, the radius of the semi-circular surface is the slot-end radius Rh , then the permanent magnet motor satisfies the relation $0.45 \leq Rh/th \leq 0.5$.

25 According to the permanent magnet motor in this case, the stress

concentration in the corner portions of the magnet slots provided in the rotor is eased, so that the effect of enabling high speed rotation of the rotor is obtained.

In a fifth aspect of the invention, the permanent magnet motor is such that the number of poles in the rotor is $2n$, and the number of salient poles in the stator is $3n$, where n is a positive integer larger than zero.

According to the permanent magnet motor in this case, where, for example, the rotor is skewed, the effect of further reducing the cogging torque is obtained.

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BRIEF DESCRIPTION OF DRAWINGS

Fig. 1 is a cross-sectional diagram of a permanent magnet motor according to an embodiment of the present invention.

Fig. 2 is a cross-sectional diagram of a rotor in the permanent magnet motor illustrated in Fig. 1.

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Fig. 3 is an enlarged partial cross-sectional diagram illustrating magnetic flux flowing from the rotor to a stator in the permanent magnet motor illustrated in Fig. 1.

Fig. 4 is a table comparing numerical values and characteristics of various components of the permanent magnet motor illustrated in Fig. 1 with a conventional interior magnet motor.

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Fig. 5 is a characteristic diagram in which the relation between td/tm and torque linearity is analyzed, where sheath thickness of the magnetic-pole portions of the rotor is tc , and magnet thickness of the permanent magnets is tm .

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Fig. 6 is a characteristic diagram in which the relation between td/tm and cogging torque is analyzed, where the sheath thickness of the magnetic-pole portions of the rotor is tc , and the magnet thickness of the permanent magnets is tm .

5 Fig. 7 is a characteristic diagram in which a magnetic field analysis of the relation between Rp/Dr and cogging torque is illustrated, where the maximum diameter of the rotor is Dr and the arc radius of the rotor is Rp .

Fig. 8 is an enlarged partial cross-sectional diagram of the outermost portion of the rotor according to another embodiment of the
10 present invention.

Fig. 9 is a characteristic diagram in which the slot ratio Rh/th , where the slot width of magnet slots is th , and the slot curvature radius of the magnet slots is Rh , and the stress relative values for the corner portion at each end of the magnet slots are analyzed.

15 BEST MODE FOR CARRYING OUT THE INVENTION

Embodiment 1.

An embodiment of the present invention will be described using Fig. 1 through Fig. 3. Fig. 1 is a cross-sectional diagram of a permanent magnet
20 motor according to the embodiment of the present invention, Fig. 2 is a cross-sectional diagram of a rotor in the permanent magnet motor illustrated in Fig. 1, and Fig. 3 is an enlarged partial cross-sectional diagram illustrating magnetic flux flow from the rotor to a stator in the permanent magnet motor illustrated in Fig. 1.

25 In Fig. 1 and Fig. 2, the permanent magnet motor 1 includes: a

stator 10 composed of a stator iron core 11 made by die-cutting thin electromagnetic steel sheets, and by laminating the electromagnetic steel sheets, and having stator coils 13 wound around twelve salient poles 11t; and an eight-pole rotor 20 having permanent magnets 31. The permanent magnet motor is configured so that the number of poles of the rotor 20 is $2n$, and the number of salient poles 11t of the stator 10 is $3n$, where n is a positive integer larger than 0, a gap g is formed between the stator 10 and the rotor 20, and when the stator coils 13 are energized, the rotor 20 is rotated by the revolving magnetic field.

The rotor 20 is a form of a chrysanthemum seal having the same number of petals as the magnetic poles, and is composed of a rotor iron core 21 that is made by die-cutting electromagnetic steel sheets having the thickness tr (not illustrated in the figure) of 0.35 (mm) into predetermined forms, to be laminated together. A hole 21y is axially bored in the center of the rotor iron core to the inside of the permanent magnets 31. Eight magnet slots 21e, whose cross-section surfaces are approximately arcuate, for engaging and fixing the permanent magnets 31, are axially bored. An inter-polar space 21a is formed between a first of the permanent magnets 31 and a second of the permanent magnets 31 that are adjacent to each other. The permanent magnets are disposed so that magnetic poles of the first of the permanent magnets 31 and the second of the permanent magnets 31 are opposites, and rotor magnetic-pole portions 24 are formed toward the stator 10 side of the permanent magnets 31, more specifically, outward of the permanent magnets 31.

The rotor magnetic-pole portions 24 are formed so that each rotor

magnetic-pole portion 24 is arcuate, with the distance from the center of the rotor iron core 21 being largest in the circumferentially central portion of the outer-side face 24c (outer peripheral shape) of each rotor magnetic-pole portion 24, and the distance from the center of the rotor iron core 21 being
5 shortest at the inter-polar space 21a between the permanent magnets 31, and are formed so that the sheath thickness t_c , which is the distance between the outer-side face of the permanent magnets 31 and the outer-side face 24c of the rotor magnetic-pole portion 24, is approximately constant, and the sheath thickness t_c is as thin as possible in consideration of die-cut
10 manufacturing.

The cross section of each permanent magnet 31 is approximately arcuate, and the magnet thickness in the radial direction of the rotor 20 is t_m .

According to the permanent magnet motor 1 configured as described
15 above, the rotor magnetic-pole portions 24 of the rotor 20 are made of electromagnetic steel sheets, so that magnetic flux Φ from the permanent magnets 31 leaks through the rotor magnetic-pole portions 24 as illustrated in Fig. 3. However, the sheath thickness t_c of the rotor magnetic-pole portions 24 in the rotor 20 is formed to be thin, so that the magnetic
20 resistance across the rotor magnetic-pole portions 24 is extremely large, and the magnetic flux leakage from the permanent magnets 31 through the rotor magnetic-pole portions 24 is small. Consequently, because the magnetic flux from the rotor magnetic-pole portions 24 comes close to saturation, the magnetic flux generated from the revolving magnetic field of
25 the stator 10 becomes hard to pass through the rotor magnetic-pole portions

24 in the rotor 20, so that the torque linearity can be enhanced.

The diameter of the rotor 20 varies as illustrated in Fig. 1 and Fig. 4 as a specific example, and the permanent magnet motor 1 is configured so that the maximum rotor diameter Dr equals 107 (mm) where the diameter of the outer-side face 24c of the rotor 20 is maximum, the rotor arc radius Rp equals 29.1 (mm), which is the radius of the circular arc formed by the outer-side face 24c of each rotor magnetic-pole portion 24, the rotor diameter ratio Rp/Dr equals 0.272, the constant thickness tc of the sheath covering the permanent magnets 31 in the outermost portion of the rotor magnetic-pole portions 24 equals 0.5 (mm), the magnet thickness tm in the radial direction of the permanent magnets 31 equals 3 (mm), and the magnet thickness ratio tc/tm equals 0.16. According to the above-described permanent magnet motor 1, the characteristics in which the cogging torque relative value is 1.0, and the torque linearity relative value is 1.059 are obtained.

In contrast, in a conventional interior permanent magnet motor, because the sheath thickness tc of the rotor magnetic-pole portions varies, given that the maximum sheath thickness tc equals 5 (mm), and the magnet thickness tm of the permanent magnets 31, the maximum rotor diameter Dr , the rotor circular arc radius Rp , and the rotor diameter ratio Rp/Dr are the same as in the permanent magnet motor 1, then the cogging torque relative value is 3.267, and the torque linearity relative value is 0.6497. Thus, the characteristics of the cogging torque and the torque linearity in the permanent magnet motor 1 are improved compared to the conventional interior permanent magnet motor.

<Torque linearity>

To begin with, the relationship between the sheath thickness t_c of the rotor magnetic-pole portions 24 and the magnet thickness t_m of the permanent magnets 31, and the torque linearity will be described according to Fig. 5. Fig. 4 is a characteristic diagram in which the relationship between the magnet thickness ratio t_c/t_m and the torque linearity is analyzed.

It is understandable that, as illustrated in Fig. 4, in order to enhance the torque linearity, the magnet thickness ratio t_c/t_m must be lowered. When the magnet thickness ratio t_c/t_m is lowered, the sheath thickness t_c of the rotor magnetic-pole portions 24 gets relatively small compared to the magnet thickness t_m , so that the magnetic flux of the rotor magnetic-pole portions 24 in the rotor 20 comes close to saturation. Consequently, the magnetic flux leakage flowing from the rotor 20 to the stator 10 decreases, so that the torque linearity can be enhanced.

<Cogging torque>

(1) Magnet thickness ratio t_c/t_m

Next, the relationship between the rotor maximum diameter D_r and the rotor arc radius R_p , and the cogging torque will be described according to Fig. 6. Fig. 6 is a characteristic diagram in which the relationship between the magnet thickness ratio t_c/t_m and cogging torque is analyzed, where the sheath thickness of the rotor magnetic pole portions is t_c , and the magnet thickness of the permanent magnets is t_m .

In Fig. 6, the cogging torque of the conventional interior permanent magnet motor is illustrated in alternate long and short dash line, and it is

understandable that, in order to lower the cogging torque of the permanent magnet motor 1 than the cogging torque of the interior permanent magnet motor, the magnet thickness ratio td/tm should be designated within a range $td/tm \leq 0.25$.

5 The cogging torque relative value is minimum where the magnet thickness ratio td/tm is around 0.158, because the magnetic flux in the rotor magnetic-pole portions 24 is saturated therearound. When the magnet thickness ratio td/tm exceeds 0.158; the cogging torque relative value increases. This is because the larger the sheath thickness tc of the rotor
10 magnetic-pole portions 24 relative to the magnet thickness tm of the permanent magnet 31, the larger the magnetic flux leakage from the permanent magnet 31 to the rotor magnetic-pole portions 24.

 The cogging torque relative value increases where the magnet thickness ratio td/tm is lower than 0.158. This is because, although the
15 smaller the sheath thickness tc relative to the magnet thickness tm , the less the magnetic flux leakage from the permanent magnets 31 to the rotor magnetic-pole portions 24, magnetic flux passing from the permanent magnets 31 through the stator iron core 11 increases, so that the cogging torque relative value increases.

20 As described above, the cogging torque of the permanent magnet motor 1 is minimum where the magnet thickness ratio td/tm is around 0.158, and the cogging torque increases as the magnet thickness ratio td/tm exceeds 0.158, and increases as the magnet thickness ratio td/tm gets smaller than 0.158.

25 If the permanent magnet motor 1 is manufactured so that the

magnet thickness ratio tc/tm equals 0.158, dimensional deviations arise in the magnet thickness tc and the sheath thickness tm . If the dimensional deviations are assumed to be 5 %, the minimum value of tc/tm is $0.158 \times 0.95 / 1.05 = 0.143$.

5 Meanwhile, the maximum value of tc/tm is $0.158 \times 1.05 / 0.95 = 0.174$.

Accordingly, by setting the magnet thickness ratio tc/tm to be within a range $0.143 \leq tc/tm \leq 0.174$, the cogging torque can be further reduced.

In addition, in order that the permanent magnet motor 1 may get characteristics in which the cogging torque relative value of the permanent
10 magnet motor 1 is about half of the cogging torque relative value of the conventional interior permanent magnet motor, the magnet thickness ratio tc/tm would be set to be within a range $0.12 \leq tc/tm \leq 0.2$.

(2) Rotor diameter ratio Rp/Dr

Next, a characteristic diagram illustrated in Fig. 7, in which a
15 magnetic field analysis of the relationship between an iron-core-rotor diameter ratio Rp/Dr and the cogging torque is illustrated, where the rotor external diameter to the outermost periphery of the rotor 20 is Dr and the arc radius of the rotor to the curved surface of each rotor magnetic-pole portion 24 is Rp , will be described.

20 In Fig. 7, the cogging torque of the permanent magnet motor 1 is minimum where the rotor diameter ratio Rp/Dr is around 0.29, because the magnetic flux wave form from the N (S) pole to the S (N) pole of the permanent magnets 31 in the rotor magnetic-pole portions 24 approximates an ideal sinusoidal wave therearound.

25 When the rotor diameter ratio Rp/Dr exceeds 0.29, as the rotor arc

radius R_p relatively increases with respect to the diameter D_r of the rotor
20, smoothness of magnetic flux variations in the sections between the
permanent magnets, in which the polarity switches from the N (S) pole to
the S (N) pole 31, is disturbed, more specifically, moves away from the ideal
5 sinusoidal wave, so that the cogging torque increases. When the
iron-core-rotor diameter ratio R_p/D_r is smaller than 0.29, as the rotor arc
radius R_p relatively increases with respect to the rotor maximum diameter
 D_r , the cogging torque increases.

The cogging torque relative value in the conventional interior
10 magnet rotor would be 0.16, where the rotor diameter ratio R_p/D_r is a
constant value 0.272.

Accordingly, in order that the cogging torque in the permanent
magnet motor 1 according to the present embodiment may be controlled to
be lower than the cogging torque in the conventional interior magnet rotor,
15 the rotor diameter ratio R_p/D_r should be set to be within a range $0.23 \leq$
 $R_p/D_r \leq 0.32$.

In addition, in order that the permanent magnet motor 1 may get
characteristics in which the cogging torque relative value of the permanent
magnet motor 1 is about half of the cogging torque of the conventional
20 interior permanent magnet motor, the rotor diameter ratio R_p/D_r would be
set to be within a range $0.255 \leq R_p/D_r \leq 0.303$.

As described above, by setting the rotor maximum diameter D_r and
the rotor arc radius R_p to be within a range $0.23 \leq R_p/D_r \leq 0.32$, and by
setting the sheath thickness t_c of the rotor magnetic-pole portions 24 to be
25 constant, and by setting the magnet thickness t_m of the permanent

magnets 31 to be 2.5 (mm) and the magnet thickness ratio t_d/t_m to be within a range $0.125 \leq t_d/t_m \leq 0.190$, the torque linearity can be enhanced, and the cogging torque can be reduced, compared to the conventional interior permanent magnet motor.

5 In addition, by setting the magnet thickness ratio t_d/t_m to be within a range $0.143 \leq t_d/t_m \leq 0.174$, the cogging torque can be further reduced.

 Moreover, because the motor is configured so that the number of poles of the rotor 20 is $2n$, and the number of salient poles 12 of the stator 10 is $3n$, when the rotor 20 is skewed, the cogging torque in the permanent magnet motor 1 can be further reduced.

Embodiment 2.

 Another embodiment of the present invention will be described according to Fig. 8. Fig. 8 is an enlarged partial cross-sectional diagram of 15 the outermost portion of the rotor according to the embodiment of the invention.

 There is a maximum rotating velocity as an important characteristic of the permanent magnet motor, other than the cogging torque and the torque linearity. The reason is that, if the maximum rotating velocity is 20 raised, a machine driven by the motor can be operated in high speed, so that productivity can be enhanced.

 However, as illustrated in Fig. 8, in the permanent magnet motor in which magnet slots 22 are provided in the rotor 20, and the permanent magnets 31 are inserted into the magnet slots 22 and fixed by adhesive 25 agents or the like, if the maximum rotating velocity is raised, the stress

concentrates in the corner portions at both ends of the magnet slots 22, whereby fixing the permanent magnets 31 can be adversely affected.

Therefore, in order to resolve the problem described above, it is conceivable that curved portions are provided in the approximately arcuate magnet slots 22 for housing the permanent magnets, axially bored in the rotor 20 as illustrated in Fig. 8, so as to reduce stress concentration.

When the length of the magnet slots 22 in the radial direction of the rotor 20 is the slot width th , an approximately semi-circular surface is formed in the corner portions at both ends of each of the magnet slots 22, and the radius of the semi-circular surface is the slot end radius Rh , the magnet slots are configured so that the slot width th equals 2.6 (mm), the slot end radius Rh equals 1.3 (mm), and the slot ratio Rh/th equals 0.5.

Next, a characteristic diagram illustrated in Fig. 9, in which the slot ratio, Rh/th , and the stress relative values at the corner portions at both ends of each of the magnet slots 22 are analyzed, will be described.

As can be seen from Fig. 9, where the slot ratio Rh/th equals 0.5, the stress relative value at the corner portions at both ends of the magnet slots 22 is minimum, and, where $0.4 \leq Rh/th$, the stress relative values at the corner portions at both ends of the magnet slots 22 are between 1.0 and 1.2, which does not cause any problem in practical use.

As described above, given that the width is th and the slot end radius is Rh , by setting Rh/th to be within a range $0.4 \leq Rh/th$, stress concentration in the corner portions at both ends of the magnet slots 22 caused by a centrifugal force due to the rotation of the rotor 20 can be reduced.

INDUSTRIAL APPLICABILITY

As described above, the permanent magnet motor relevant to the present invention is suitable for a synchronous motor, for instance.